

# **Heat pumps and their role in the decarbonising of heat**

CIBSE North-east region technical meeting, January 2018

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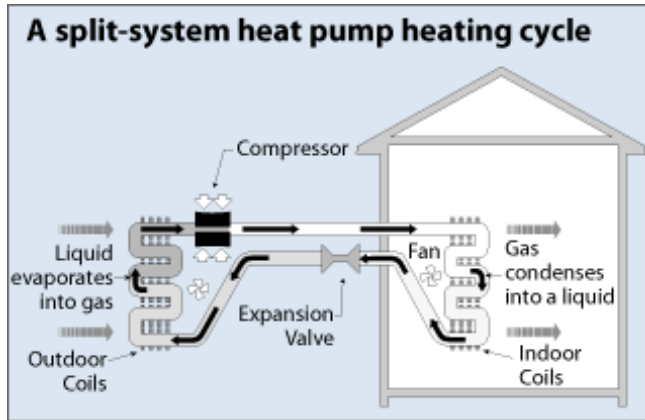
# Outline

- First, how can we use them why should we get interested in heat pumps
- Next, a technology review
- The potential of heat pumps to reduce carbon emissions will be demonstrated
- Current technology however is not living up to this promise – reasons will be explored
- A look at some of the research and engineering practice questions that might be posed to address performance shortcomings
- A look at some examples of how the technology might be exploited in future

# A future for heat pumps?

- There is a growing need to reconsider the means by which we deliver domestic space and hot water heating in the UK in order to...
  - Reduce carbon emissions
  - Diversify from an over-dependence on gas
  - Arrest the alarming rise in fuel poverty
- The government likes to call this its *energy trilemma*
- It will be shown that heat pumps have the potential to address all of the above
- They are expected to play an increasing role in the search for alternatives to conventional gas boiler-based heating

# Vapour compression cycle – accounts for >90% of heat pumps worldwide

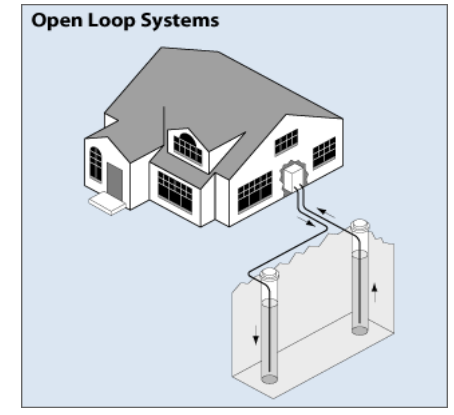
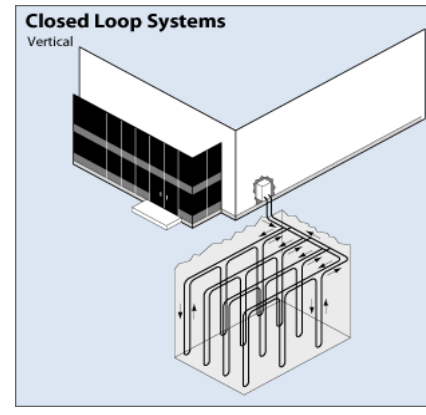
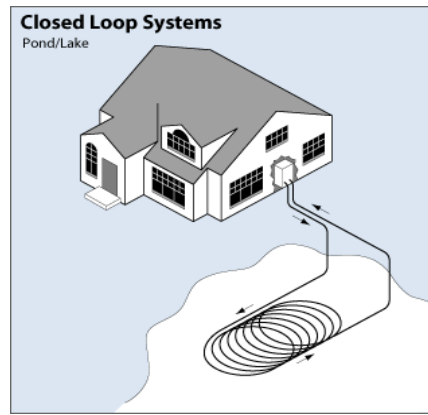
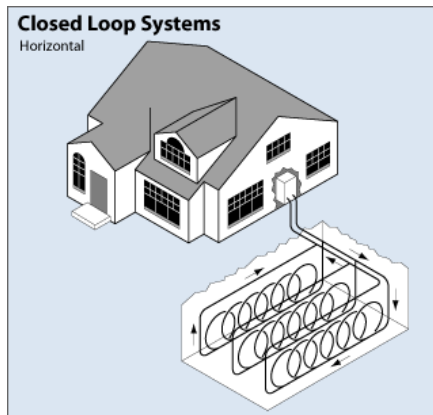


According to the First Law:  $Q_c = Q_e + W_c$

Practical cycle, for a heat pump:  $CoP = Q_c / W_c = Q_c / (Q_c - Q_e)$

$CoP_{\text{Refrigerator}} = Q_e / W_c = (Q_c - W_c) / W_c = (Q_c / W_c) - 1 = CoP_{\text{HeatPump}} - 1$

That is:  $CoP_{\text{HeatPump}} = CoP_{\text{Refrigerator}} + 1$



(Figures reproduced courtesy of the US DOE Office of Energy Efficiency and Renewable Energy)

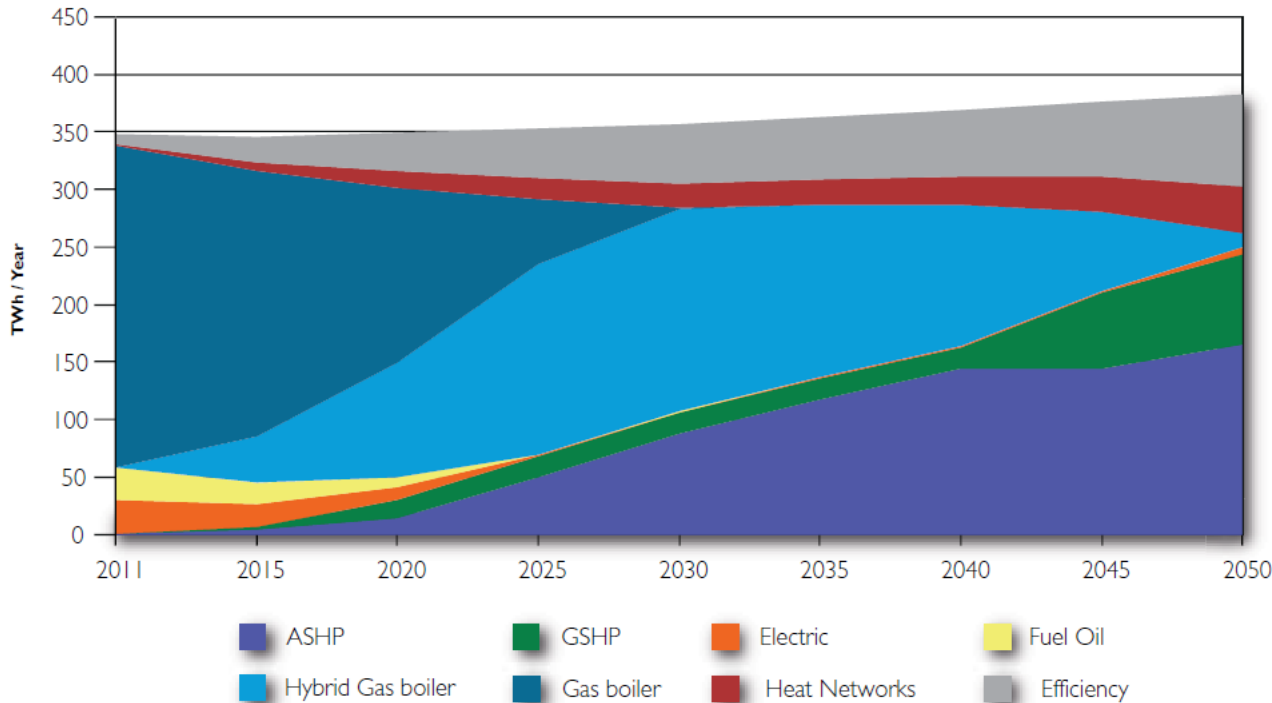
## So what?

- In the UK alone 300,000 domestic gas boilers are replaced every year.
- At best, each operates at a seasonal mean efficiency of 0.92 (\*).
- Each will discharge  $0.184/0.92 = 0.2\text{kg}$  of  $\text{CO}_2$  to the atmosphere per unit of energy delivered to the connected heating system (\*\*).
- Today in the UK, a heat pump, operating with a *CoP* of 3, will discharge  $0.352/3 = 0.117\text{kg}$  of  $\text{CO}_2$  – nearly 42% less than the best gas boiler.
- In 2015, the same heat pump would have discharged 0.15kg of  $\text{CO}_2$  – 25% less than the gas boiler
- The reduction in  $\text{CO}_2$  emission since 2015 is the result of the electricity grid decarbonising in the meantime

\* Recent surveys suggest that as many as 90% of UK domestic gas boilers rarely condense which means that their seasonal efficiencies are more likely to be around 0.85.

\*\* <https://www.gov.uk/government/publications/greenhouse-gas-reporting-conversion-factors-2017> (accessed 7th August 2017)

# UK domestic space and hot water energy by technology to 2050



(Notwithstanding fracking, the pressure is on to diversify away from gas for those countries without indigenous reserves)

Source: *The future of heating: Meeting the challenge*. London: Department of Energy and Climate Change.

[Online] Available at:

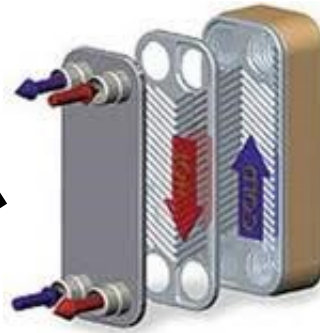
[https://www.gov.uk/government/uploads/system/uploads/attachment\\_data/file/190149/16\\_04-DECC-The\\_Future\\_of\\_Heating\\_Accessible-10.pdf](https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/190149/16_04-DECC-The_Future_of_Heating_Accessible-10.pdf)

(accessed November 2014)

# Heat pumps – a review of the technology

# Well established 1<sup>st</sup> and 2<sup>nd</sup> generation technologies...

Brazed plate condenser  
(typical 'pinch' 2-3K)



Mechanical thermostatic  
expansion valve

Working fluids – R134a or  
zeotropic blends R407C, R410A



Water source - brazed  
plate evaporator  
(typical 'pinch' 2-3K)

OR



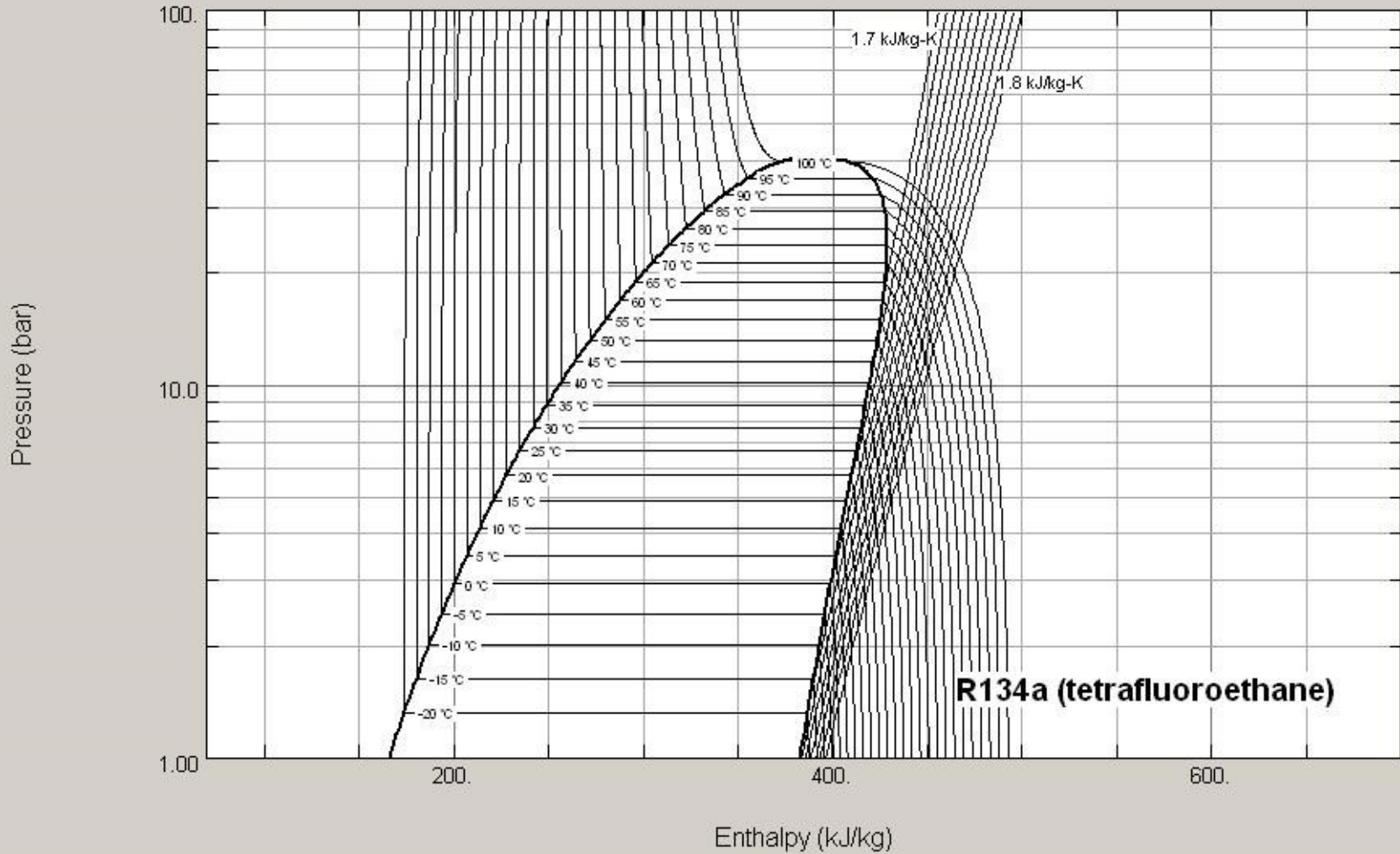
Air source – fin-and-coil  
Evaporator (typical 'pinch'  
3-5K)



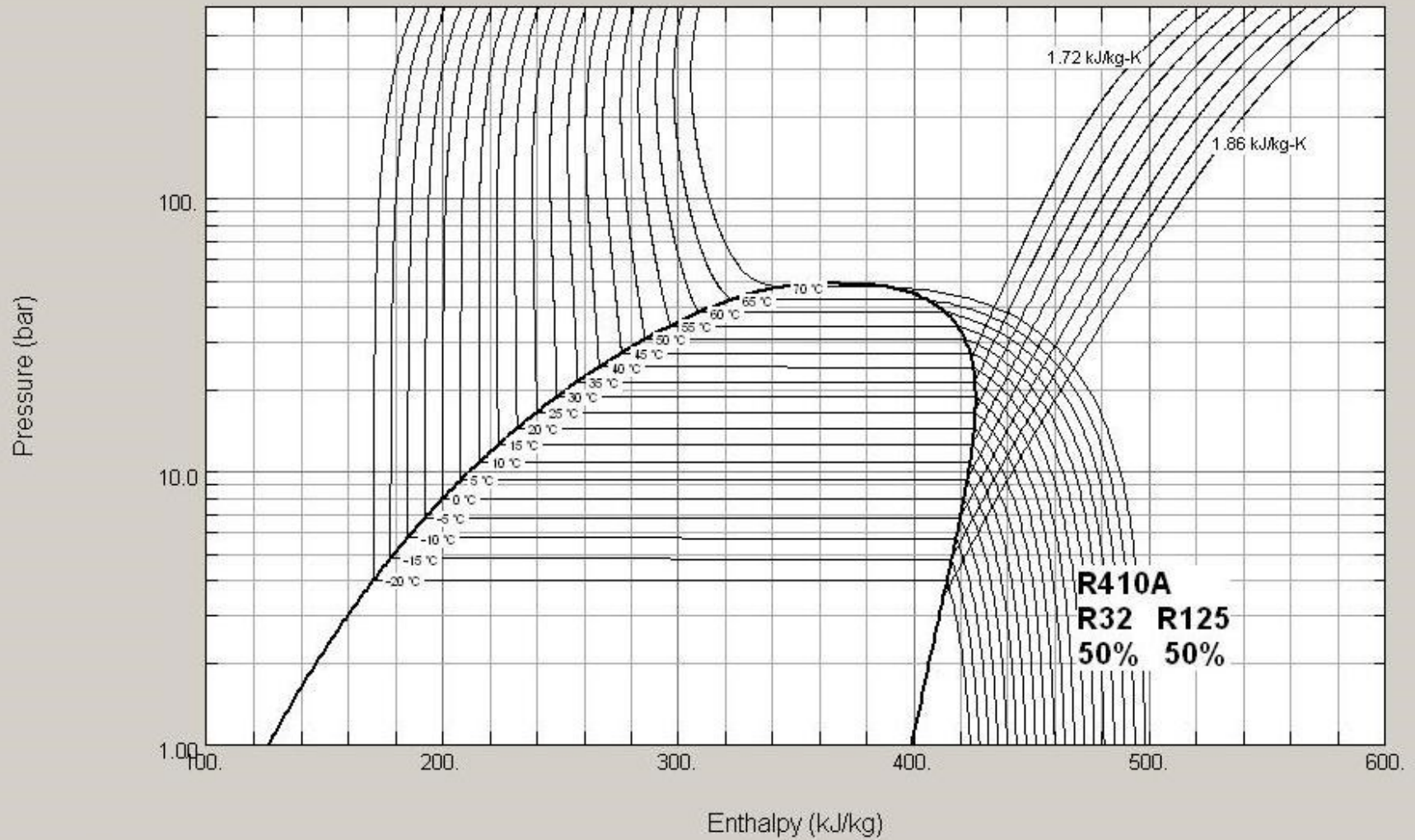
Scroll  
compressor



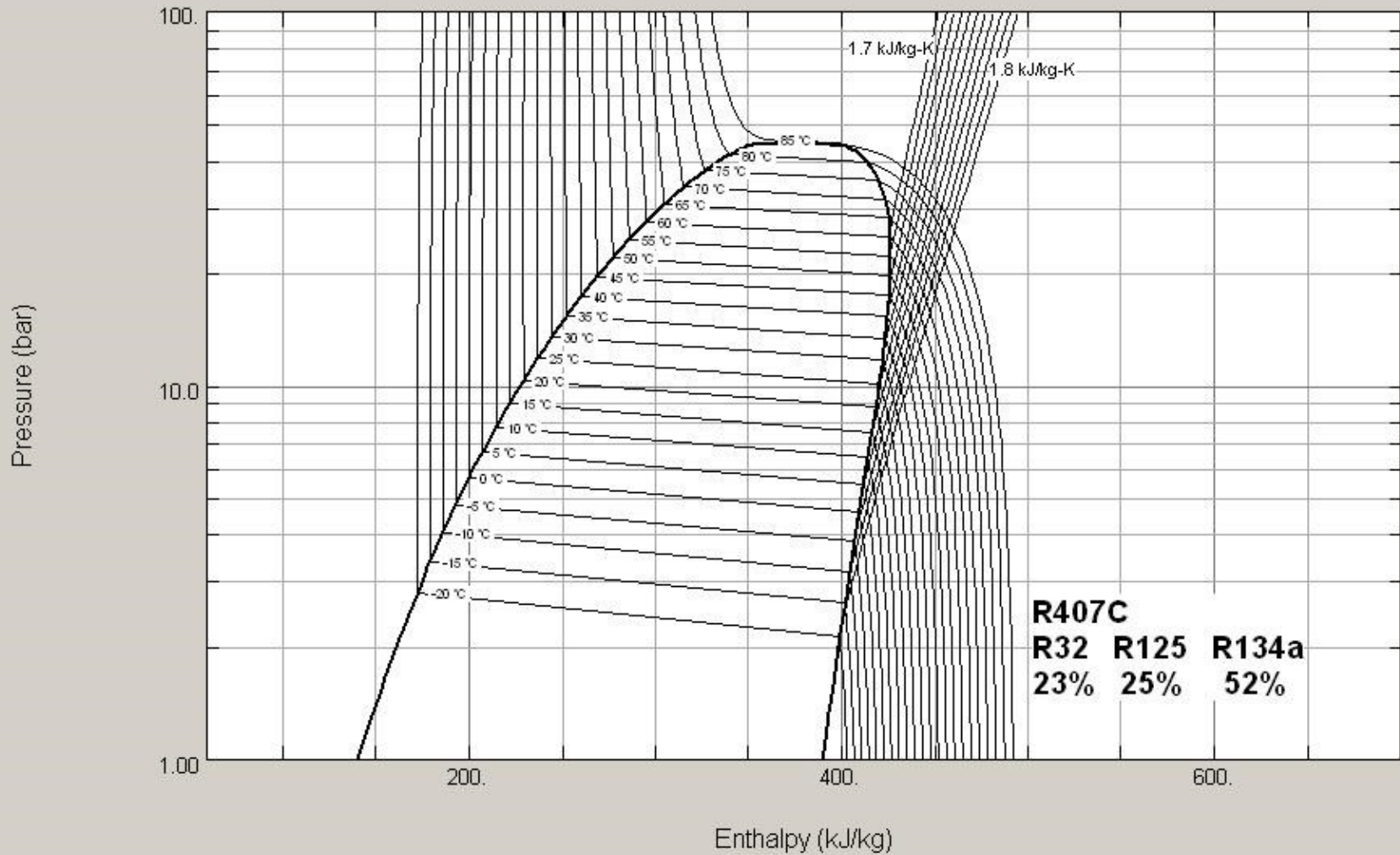
# Working fluids – pure fluid R134a



# Working fluids – binary near-azeotrope blend R410A



# Working fluids – ternary zeotropic blend R407C

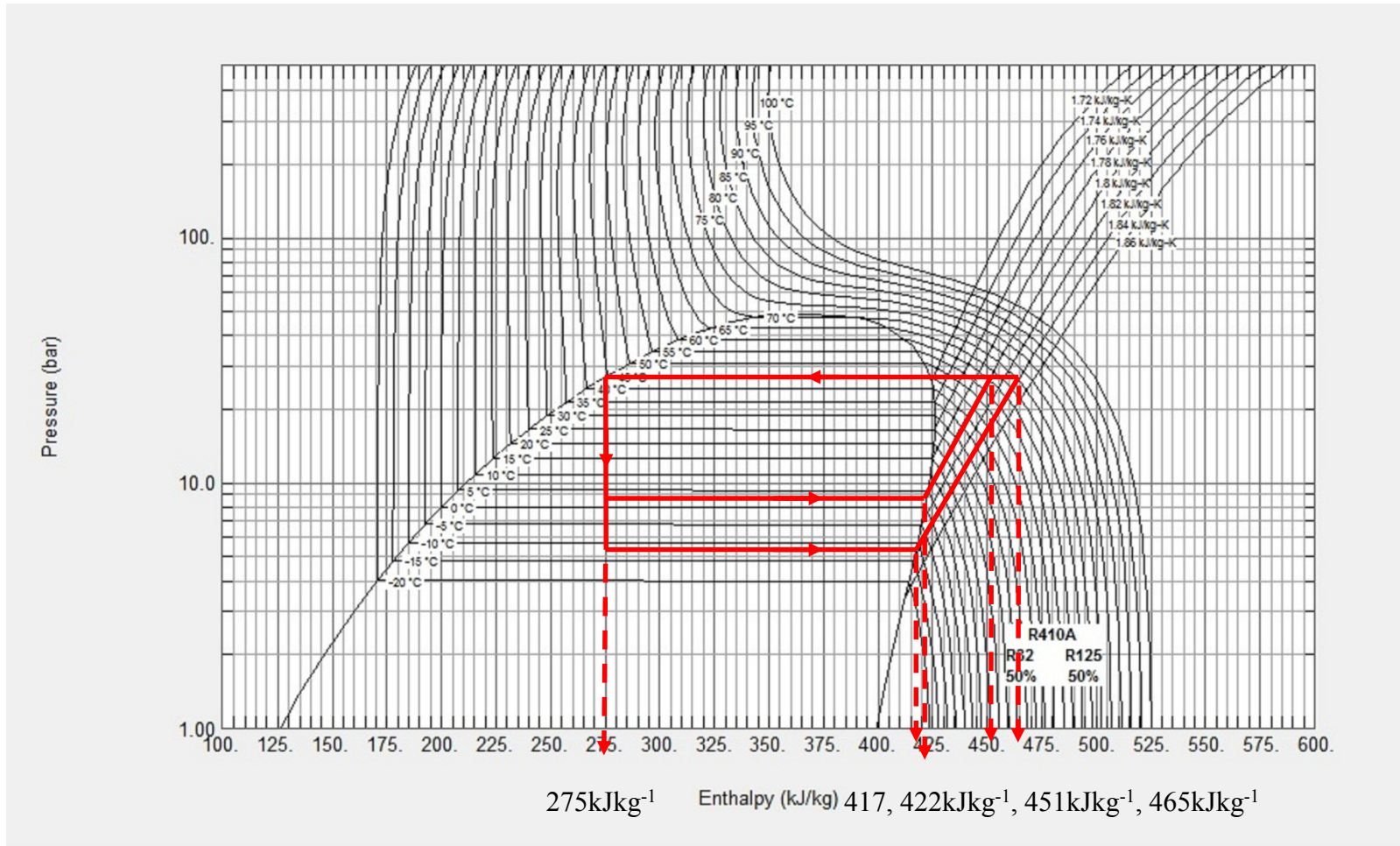


## Common working fluids compared

FLUID	TYPE	GWP (*)	COMMENT
R134a	Organic HFC	1430	Mainly commercial
R407C	Organic HFC blend	1774	Domestic/commercial
R410A	Organic HFC blend	2088	Domestic/commercial
R32	Organic HFC	675	Not yet widespread; flammability
R290	Organic HC	3.3	Mainly process; flammability
R717 (ammonia)	Inorganic	?	Toxicity
R744 (CO <sub>2</sub> )	Inorganic	1	Low critical temperature

\*Global warming potential – the global warming effect with reference to CO<sub>2</sub>

# Theoretical performance

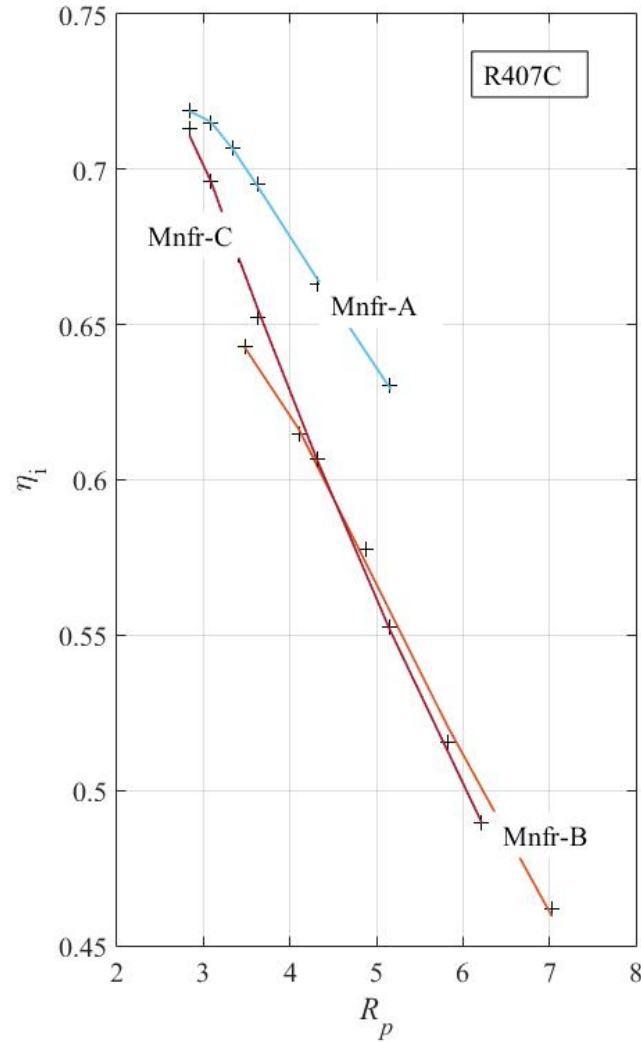
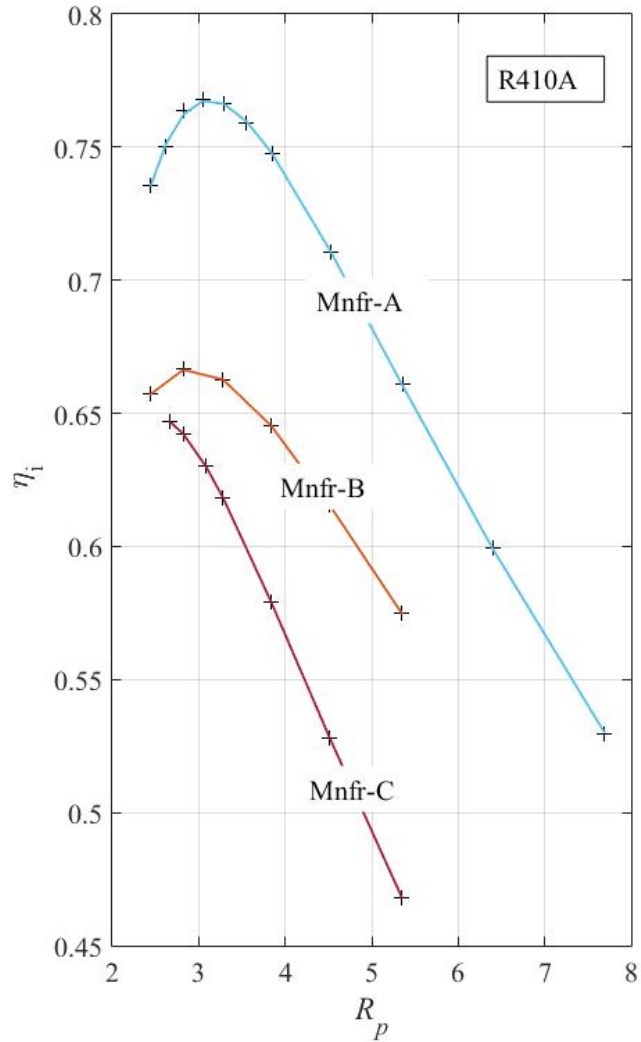


For an overall compressor isentropic efficiency of 0.65...

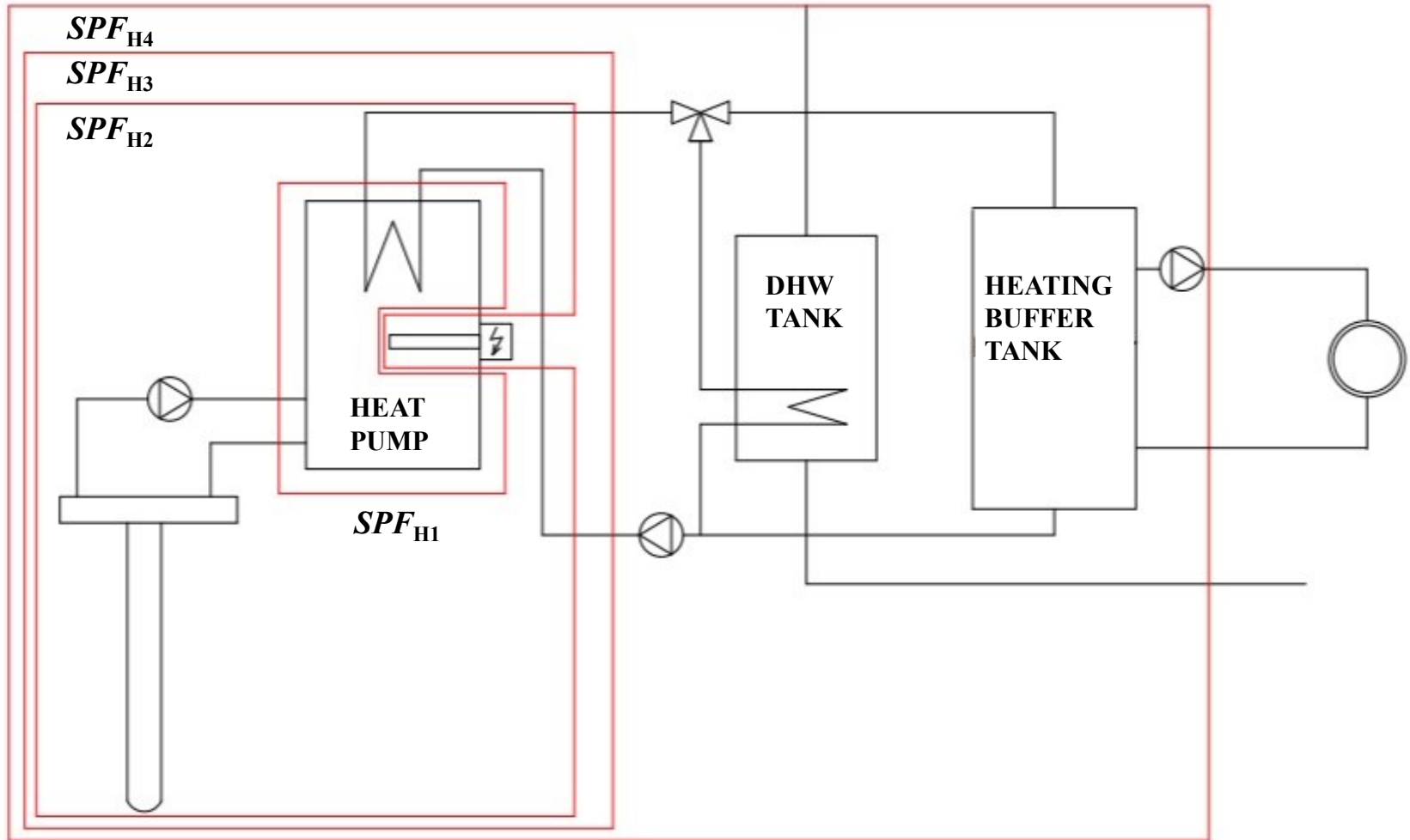
$$\text{Ground source: } CoP = 0.65 \times \frac{451 - 275}{451 - 422} = 3.9 \quad \text{Air source: } CoP = 0.65 \times \frac{465 - 275}{465 - 417} = 2.6$$

(Typically, the source pump will reduce  $CoP_{GS}$  by up to 5% and the source fan  $CoP_{AS}$  by up to 10%)

# Typical compressor efficiencies are key

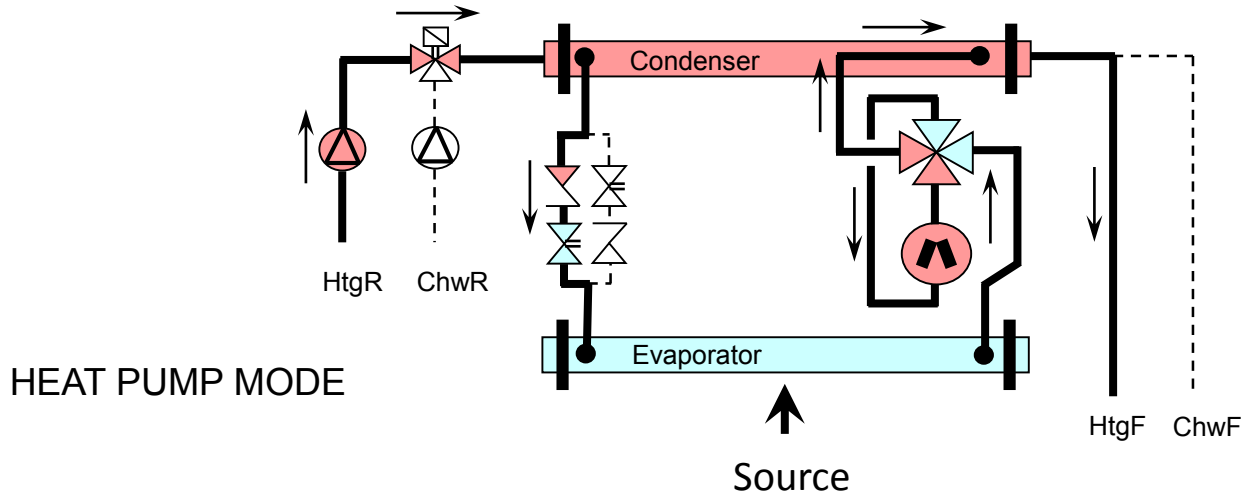


# Seasonal performance factor, $SPF$ vs. $CoP$

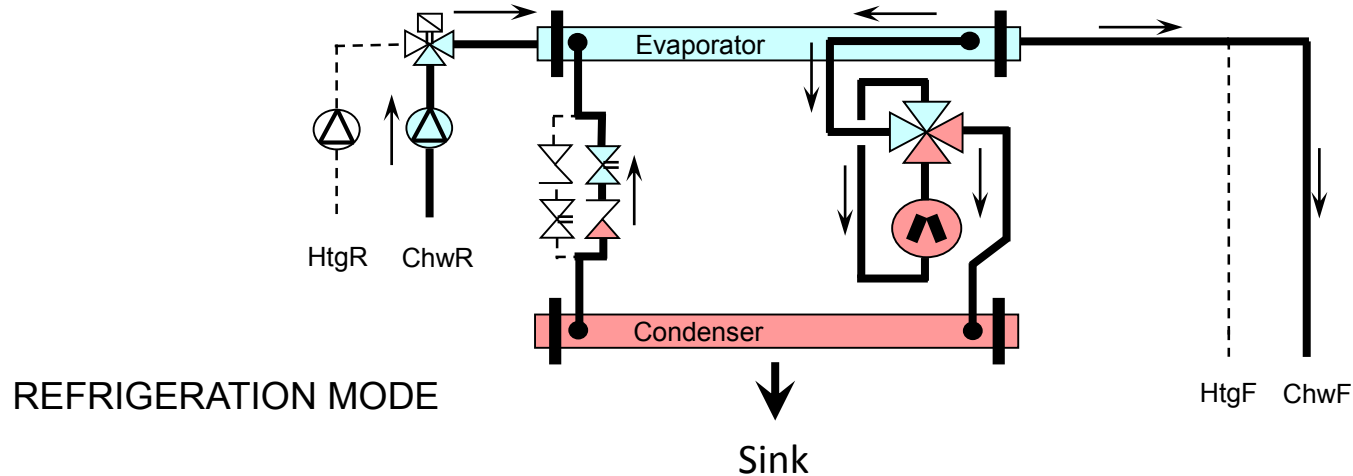


e.g.  $SPF_{H3} = (Q_c + E_{\text{cassette}}) / (W_{\text{HP}} + W_{\text{src pump}} + E_{\text{cassette}})$

# Reverse cycling for air conditioning and defrosting



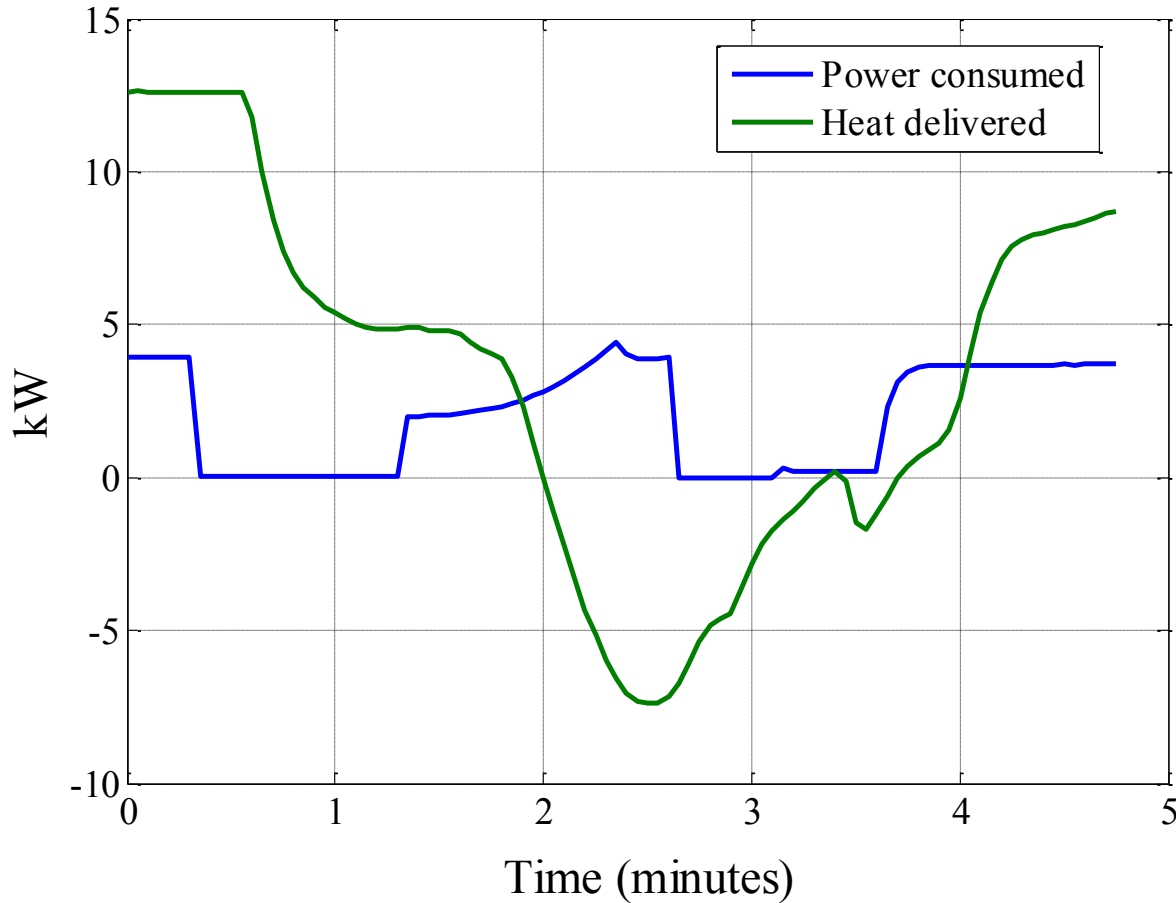
These refinements permit the same plant to operate as a heat pump in winter and an air-conditioner in summer.





# Defrosting in air-source heat pumps

DEFROST EVENT DYNAMICS - POWER AND HEAT



(Typical domestic heat pump example)

Periodic defrosting is needed in air-source heat pumps. In UK conditions this will typically arise at external air temperatures  $< 7^{\circ}\text{C}$ .

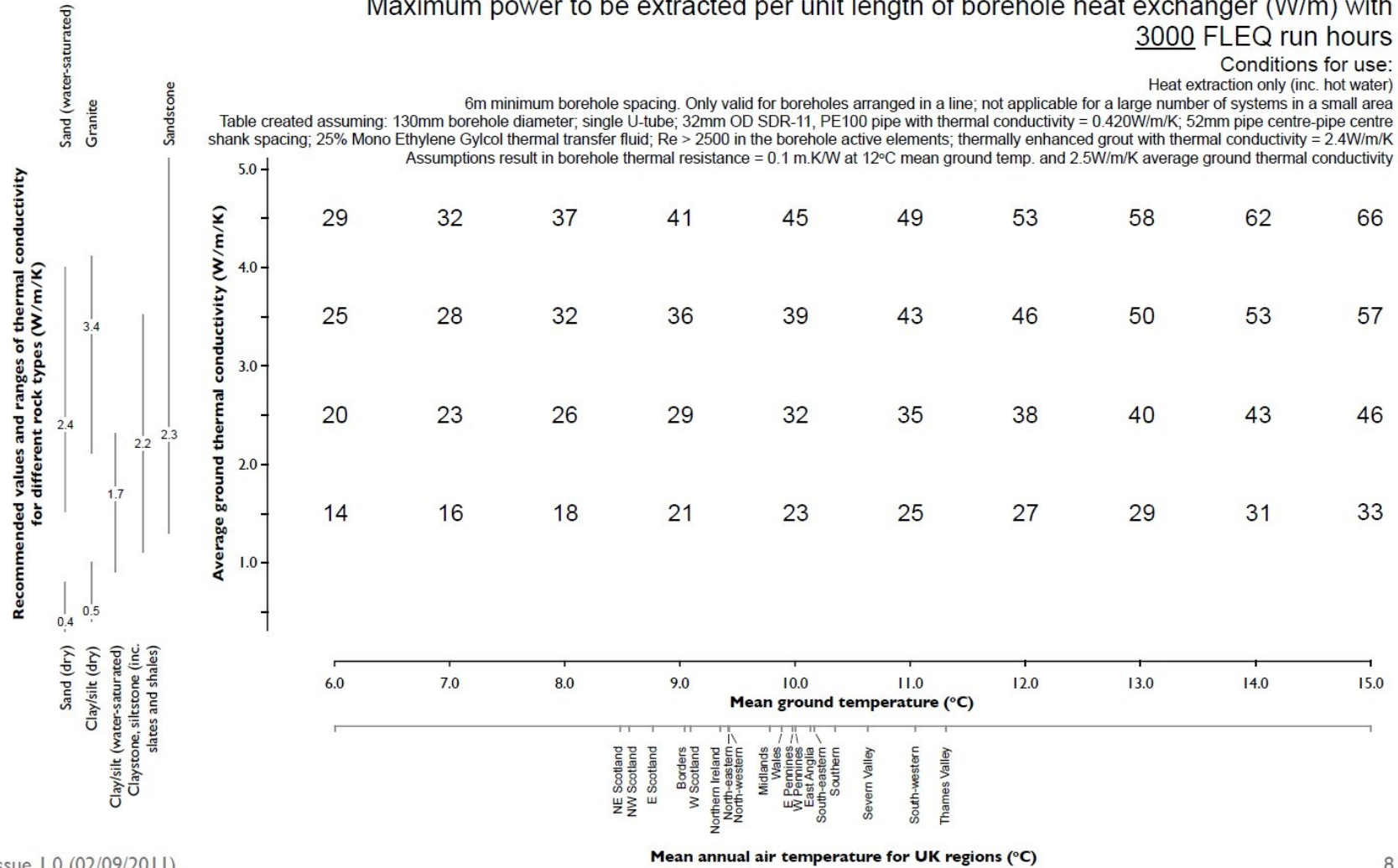
At these lower external temperatures, the refrigerant in the evaporator drops to below  $0^{\circ}\text{C}$ . Thus, water condensing in the air being cooled across the evaporator subsequently turns to ice as it settles on the evaporator surface. Typically in UK conditions, defrosting will add a 8-10% 'overhead' on annual power consumption.

# Ground sourcing alternative – typical array capacities

Maximum power to be extracted per unit length of borehole heat exchanger (W/m) with 3000 FLEQ run hours

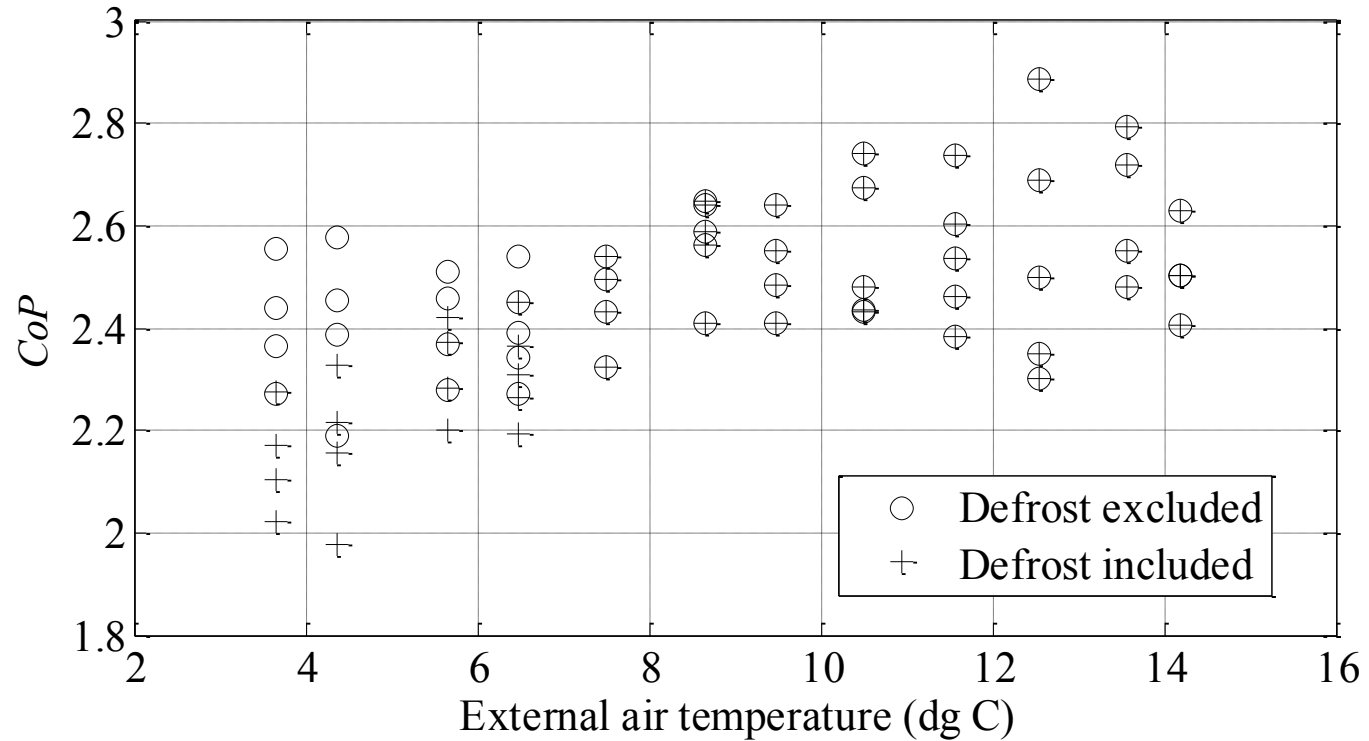
Conditions for use:  
Heat extraction only (inc. hot water)

6m minimum borehole spacing. Only valid for boreholes arranged in a line; not applicable for a large number of systems in a small area  
Table created assuming: 130mm borehole diameter; single U-tube; 32mm OD SDR-11, PE100 pipe with thermal conductivity = 0.420W/m/K; 52mm pipe centre-pipe centre shank spacing; 25% Mono Ethylene Glycol thermal transfer fluid; Re > 2500 in the borehole active elements; thermally enhanced grout with thermal conductivity = 2.4W/m/K  
Assumptions result in borehole thermal resistance = 0.1 m.K/W at 12°C mean ground temp. and 2.5W/m/K average ground thermal conductivity

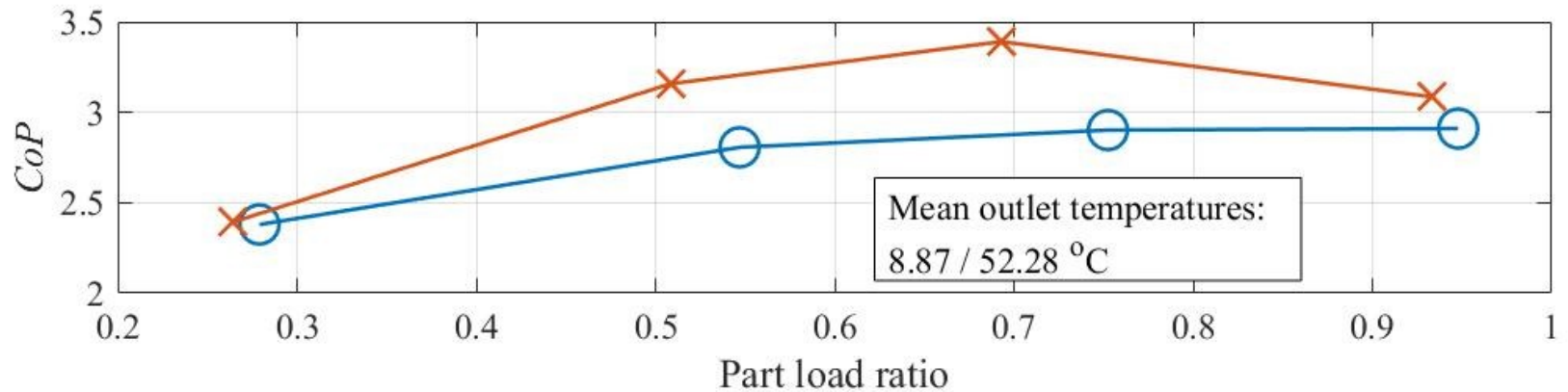
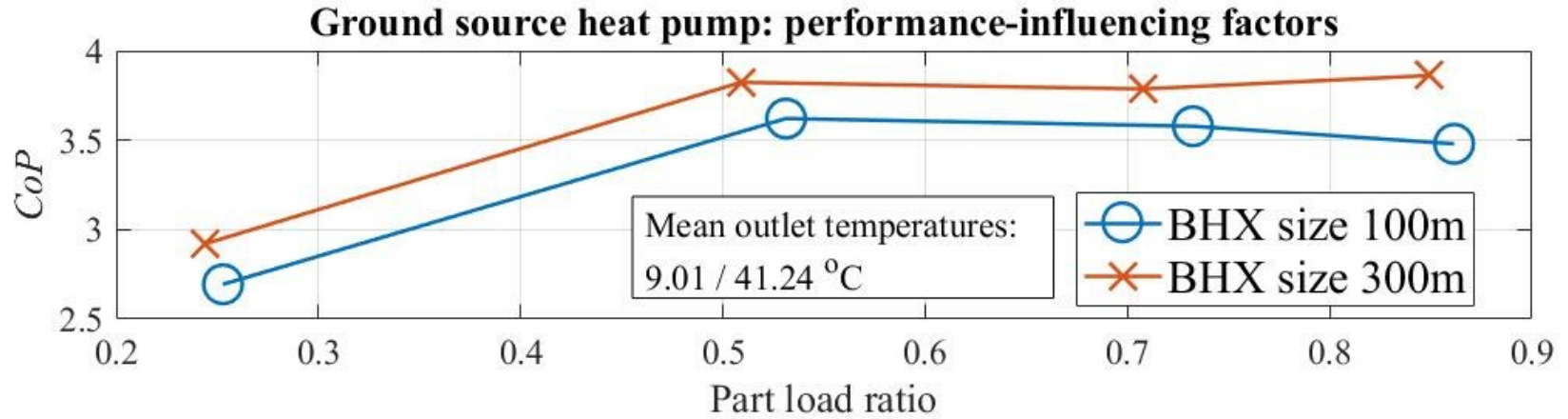


# Performances in practice

# Practical performances – air-source

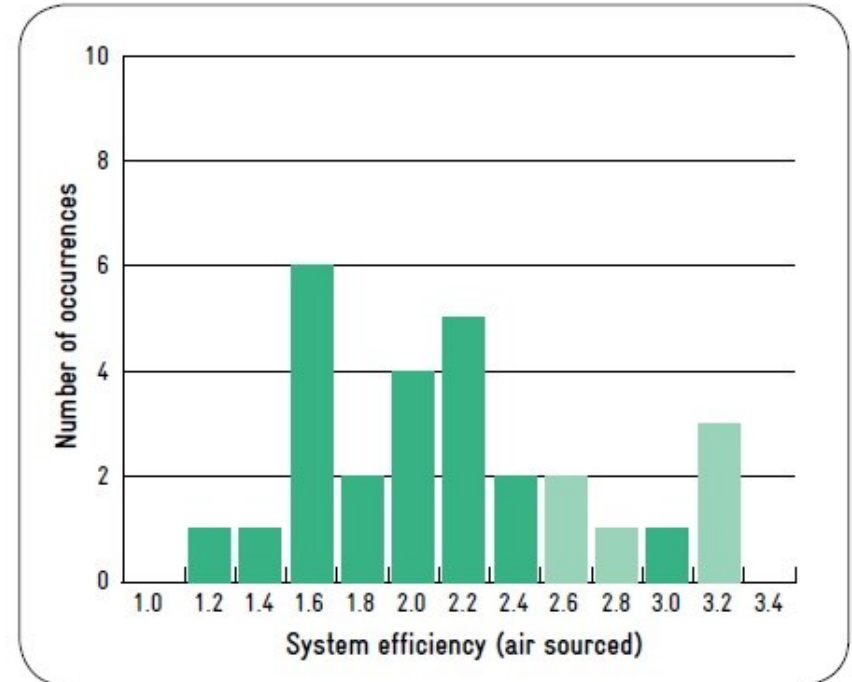
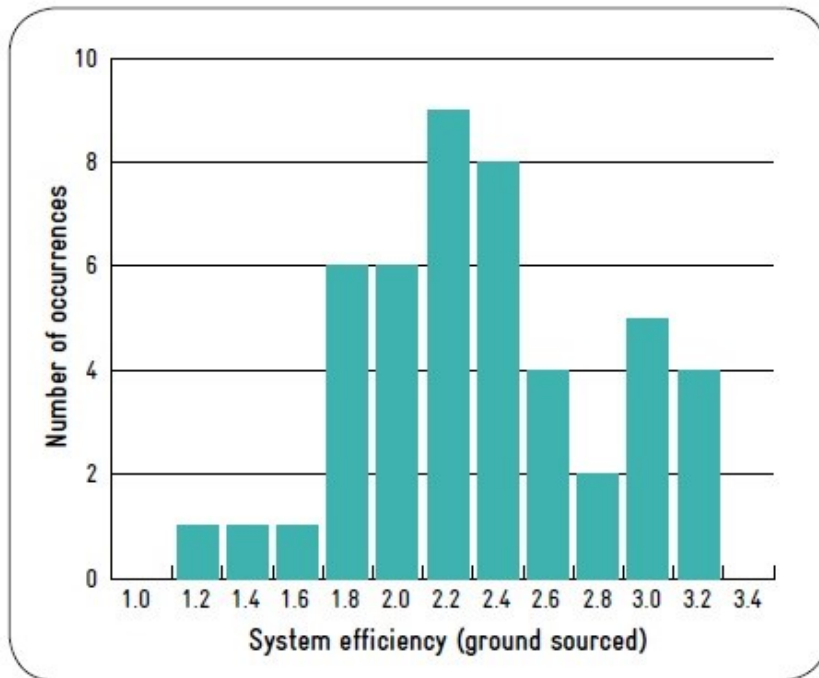


# Practical performances – ground-source



# Field-trialled UK performances

First year (2009/10) results of UK field trials conducted at 82 domestic sites of ground- and air-source heat pumps...

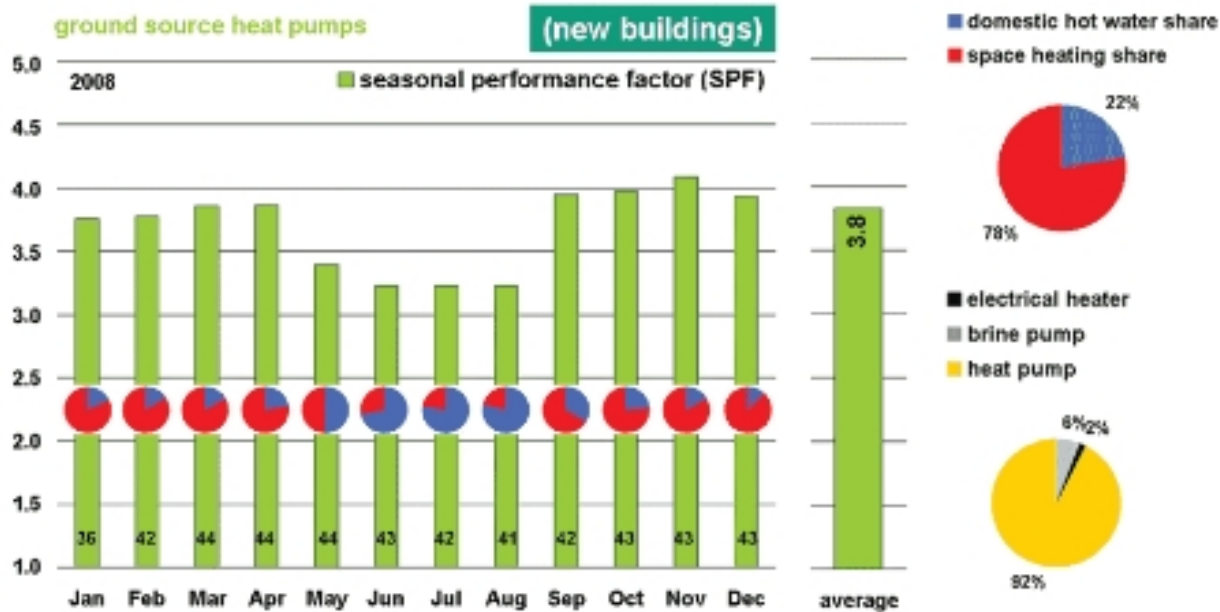


Source: *Getting warmer: a field trial of heat pumps*. London: The Energy Saving Trust.

[Online] Available at: <http://www.heatpumps.org.uk/PdfFiles/TheEnergySavingTrust-GettingWarmerAFieldTrialOfHeatPumps.pdf>

(accessed December 2013)

# Compared with Germany...



This shows results obtained by the Fraunhofer Inst. from 68 German ground source heat pumps in new low energy houses, the majority (93%) of which used underfloor heating. The annual mean *SPF* is 3.8. For air source heat pumps the annual *SPF* was 2.9 (new houses) and 2.6 (existing); the main differences being the lower insulation standard and the predominant use of radiator heating in the existing houses.

Source: Miara, M. (2009). *Heat Pumps in Action*. RenewableEnergyWorld.com. [Online] Available at: <http://www.renewableenergyworld.com/rea/news/article/2009/10/heat-pumps-in-action> (accessed November 2014)

# SPFs compared

COUNTRY	SOURCE	SITES	MEAN
Sweden	Ground	6	3.26
Germany - existing	Ground	36	3.30
Germany - new build	Ground	56	3.88
UK phase 1 trials	Ground	49	2.31
UK phase 2 trials	Ground	21	2.82
BEIS/UCL RHPPP trials	Ground	223	2.75
Germany - existing	Air	34	2.60
Germany - new build	Air	18	2.89
UK phase 1 trials	Air	22	1.83
UK phase 2 trials	Air	15	2.45
BEIS/UCL RHPPP trials	Air	76	2.30

Gleeson, C.P., & Lowe, R. (2013) Meta-analysis of European heat pump field trial efficiencies. *Energy and Buildings* 66, 637-47.

*Getting Warmer – a Field Trial of UK Domestic Heat Pumps*. Energy Saving Trust, UK. [Online] available at: <http://www.heatpumps.org.uk/PdfFiles/TheEnergySavingTrust-GettingWarmerAFieldTrialOfHeatPumps.pdf>

*The heat is on: Heat pump field trials phase 2*. UK: Energy Saving Trust, UK. [Online] available at: [https://www.gov.uk/government/uploads/system/uploads/attachment\\_data/file/225825/analysis\\_data\\_second\\_phase\\_est\\_heat\\_pump\\_field\\_trials.pdf](https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/225825/analysis_data_second_phase_est_heat_pump_field_trials.pdf)

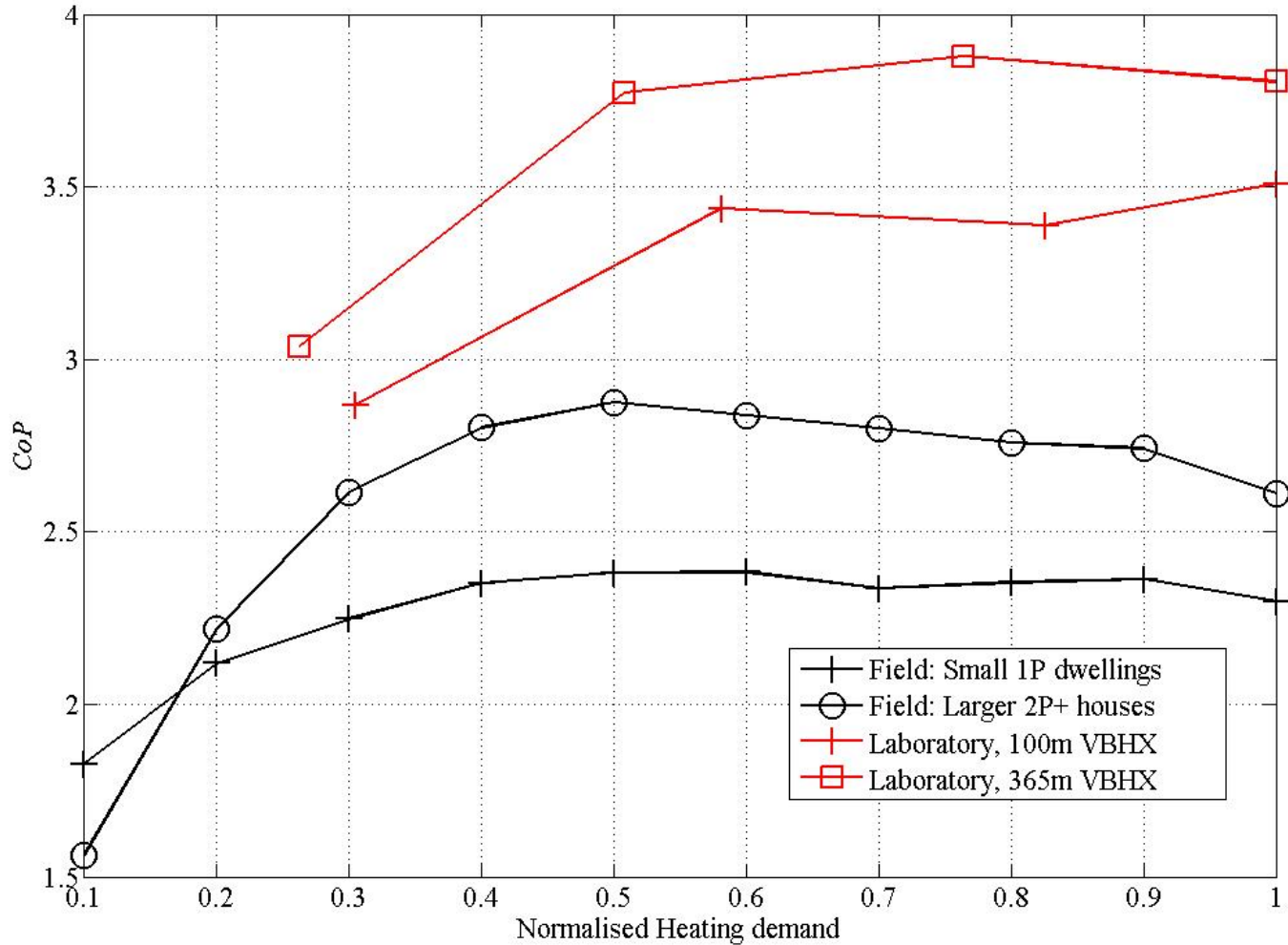
DECC, Detailed analysis of data from heat pumps installed via the Renewable Heat Premium Payments Scheme, 2017, [On <https://www.gov.uk/government/publications/detailed-analysis-of-data-from-heat-pumps-via-the-renewable-heat-premium-> (Accessed 18 August 2016)



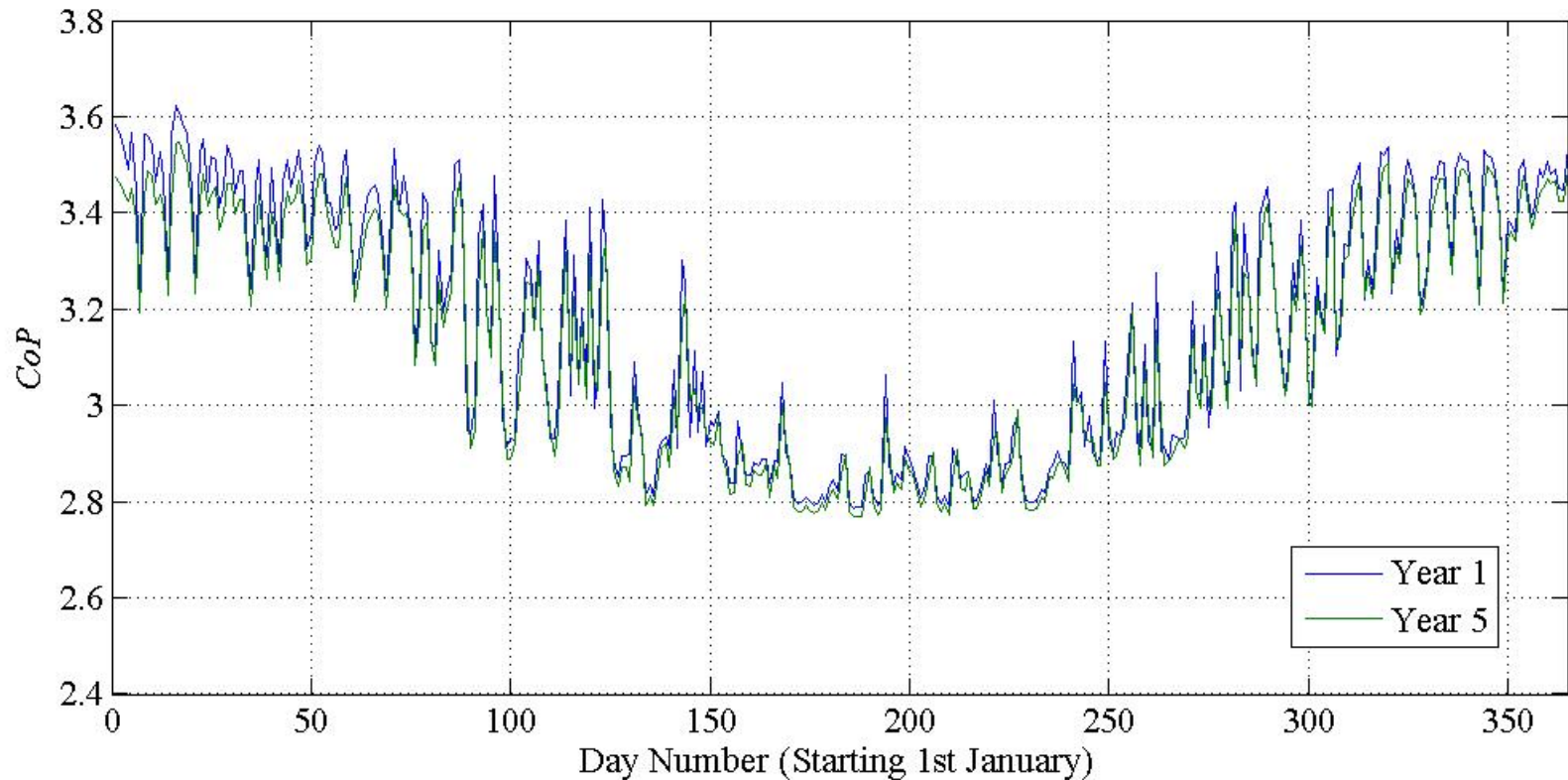
# So why do UK systems perform so badly?

- Sizing of the heat pump itself – risk-averse design the main culprit.
- Sizing of the array (ground-source).
- Control factors – defrosting (air-source); inappropriate (or lack of) use of weather-compensating control.
- Choice of heating – underfloor versus radiators (especially problematical in retrofit applications).
- Thermostatic controls (especially with inappropriate buffering)
- Domestic hot water storage temperatures and tank pasteurisation.

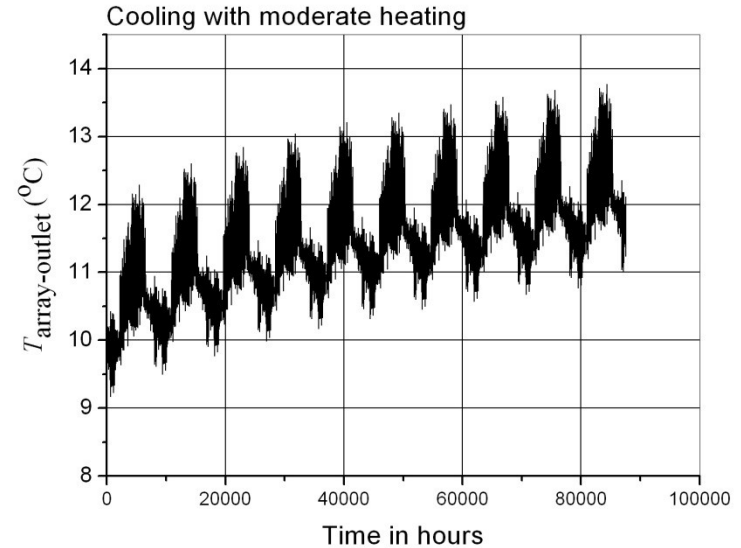
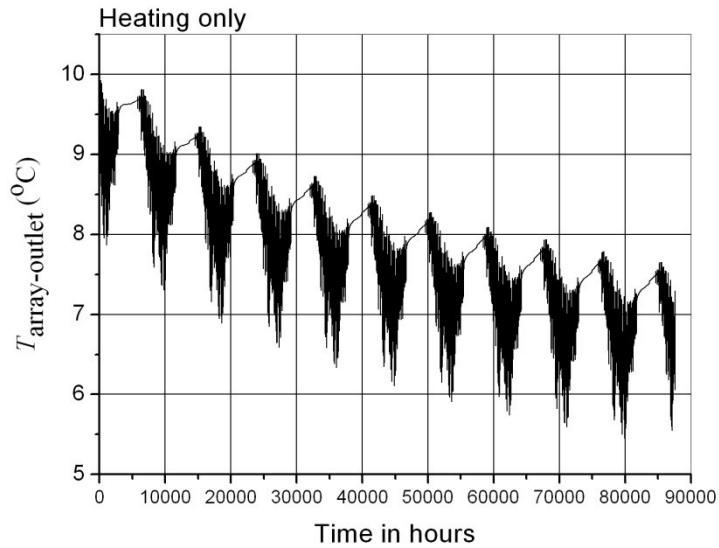
# Part-load performances



# Part load problems also evident during summer months even with good heat pump sizing...



# Impact of poorly-sized sized array (ground-source)



# Social factors\*

- The highest 10% of gas users consume four times as much as the lowest 10% but are unaware of this.
- About 40% of this variation can be explained by physical factors (property type, age, size, insulation standard).
- A major part of the remaining 60% is due to social factors – how the occupants behave (comfort temperature choice; time spent at home; use of windows, etc).
- Even the lowest 10% have the potential to reduce energy use without affecting comfort.

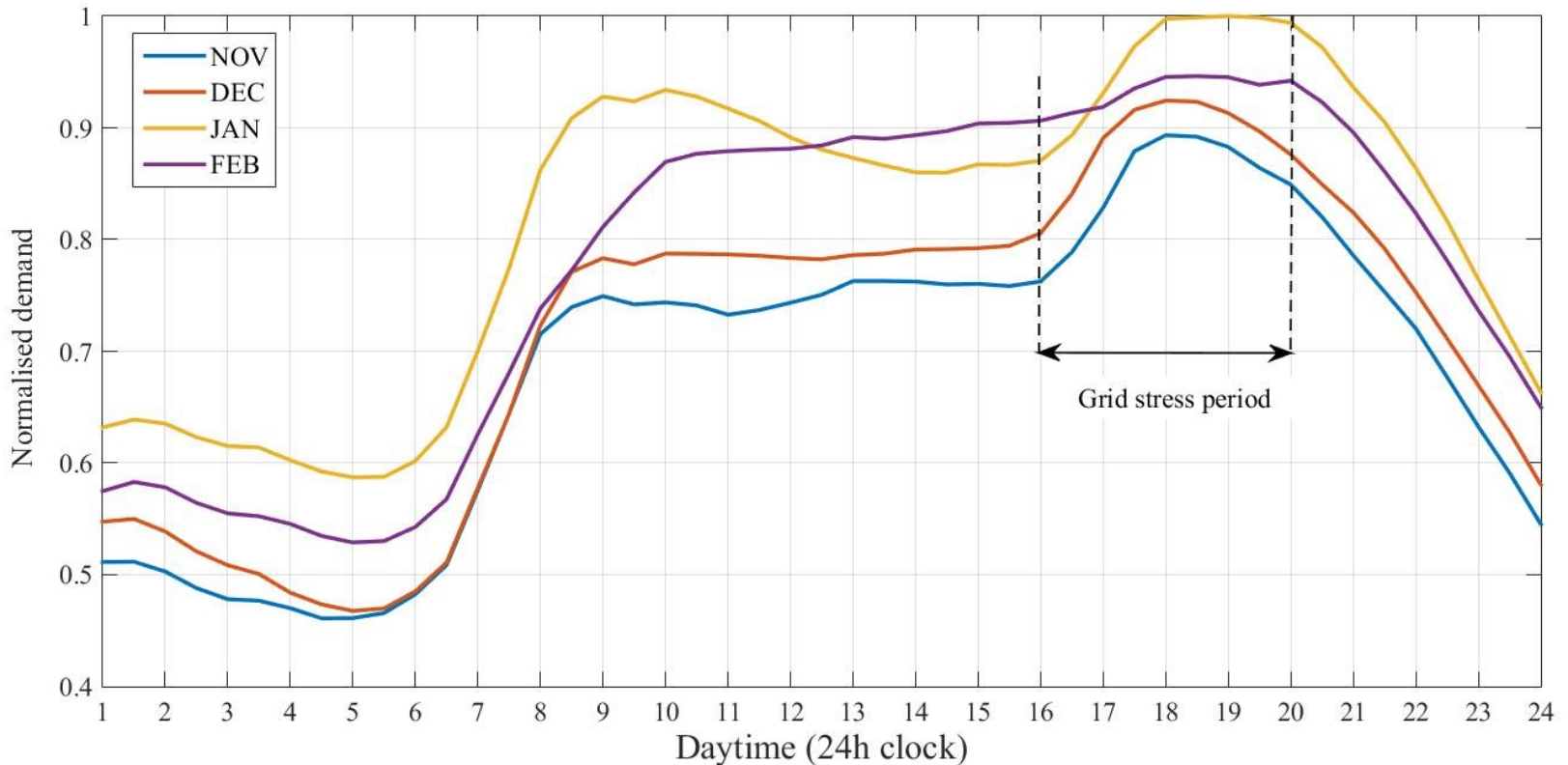
\* Fell, D. & King, G. (2012). *Domestic energy use study: To understand why comparable households use different amounts of energy*. London: DECC.

## **Some challenges for the future**

# Where now? (Suggestions for further R & D)

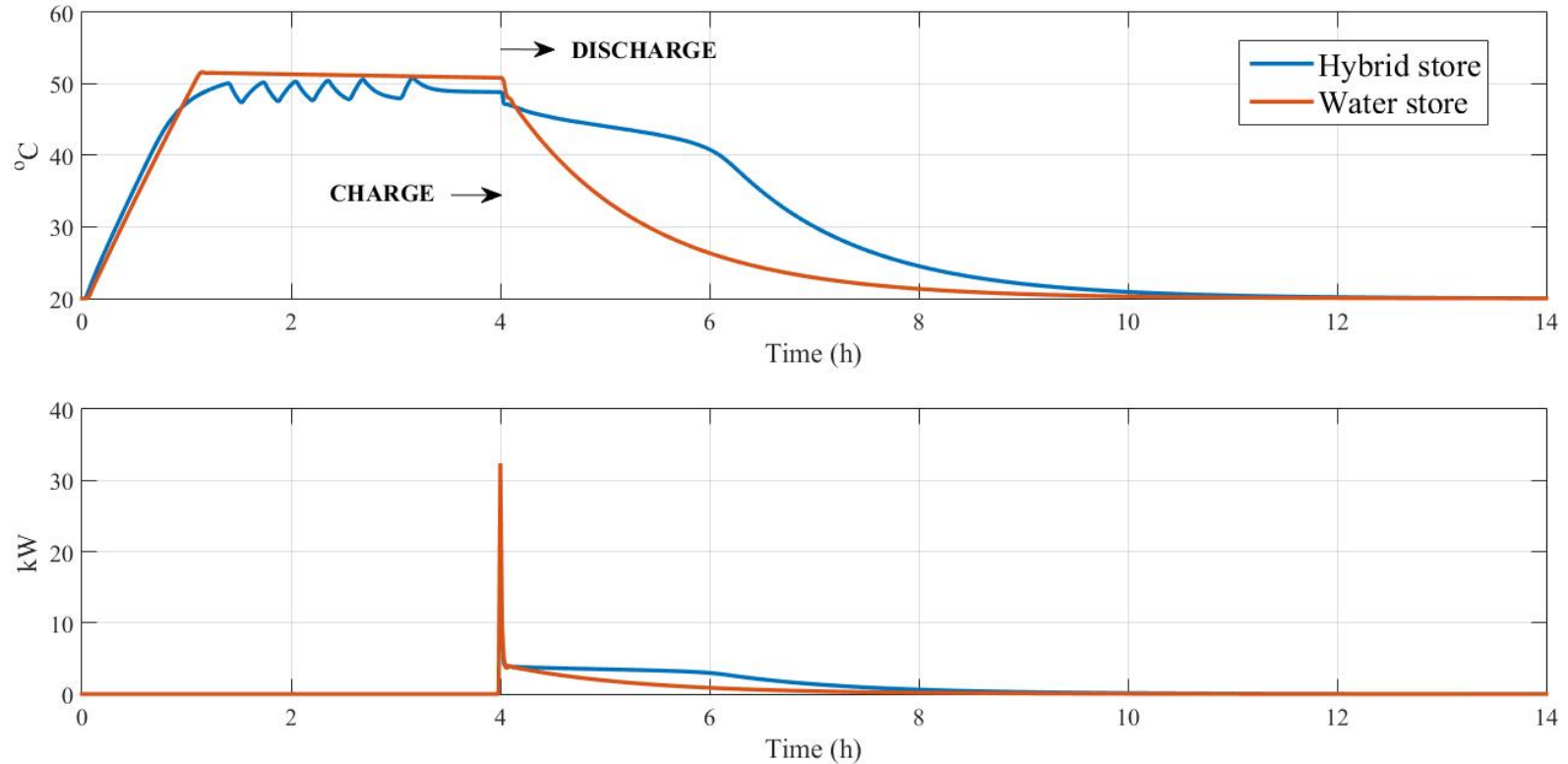
- The *potential* for ground source heat pumps to reduce household energy bills and deliver carbon savings has been shown to be excellent and the market size is substantial.
- Existing performances in the field are not good enough – earlier slides have shown that seasonal *CoPs* must be at least 3 to be viable.
- Between 1995 and 2003, domestic heat pump efficiencies improved by 20% due to continuous product improvement during those years (Gleeson & Lowe – slide 24).
- Though there are numerous reasons for poor performances in the field, the following issues are repeatedly mentioned...
  - Heat pump sizing – in particular the avoidance of over-sizing (consider the use of dynamic thermal modelling to size the heat pump rather than current practice which uses a steady-state energy balance with ‘worst case’ boundary conditions).
  - Heat pump technology – a rapid move to 3<sup>rd</sup> generation technology using variable speed compressor drives and electronic expansion devices is needed.
  - Heat pump integration – increased buffering through the use of phase change materials.
  - System controls – life beyond the thermostat can be found using AI methods the most promising of which for this type of problem is fuzzy set theory.
  - Ground array design – simulation tools are maturing and becoming robust and reliable but most have impracticable computational demands; simplified but reliable design-sizing tools such as ‘g-functions’ need to become more widely available for practitioners.

# The challenge of grid stress – grid reinforcement or storage?



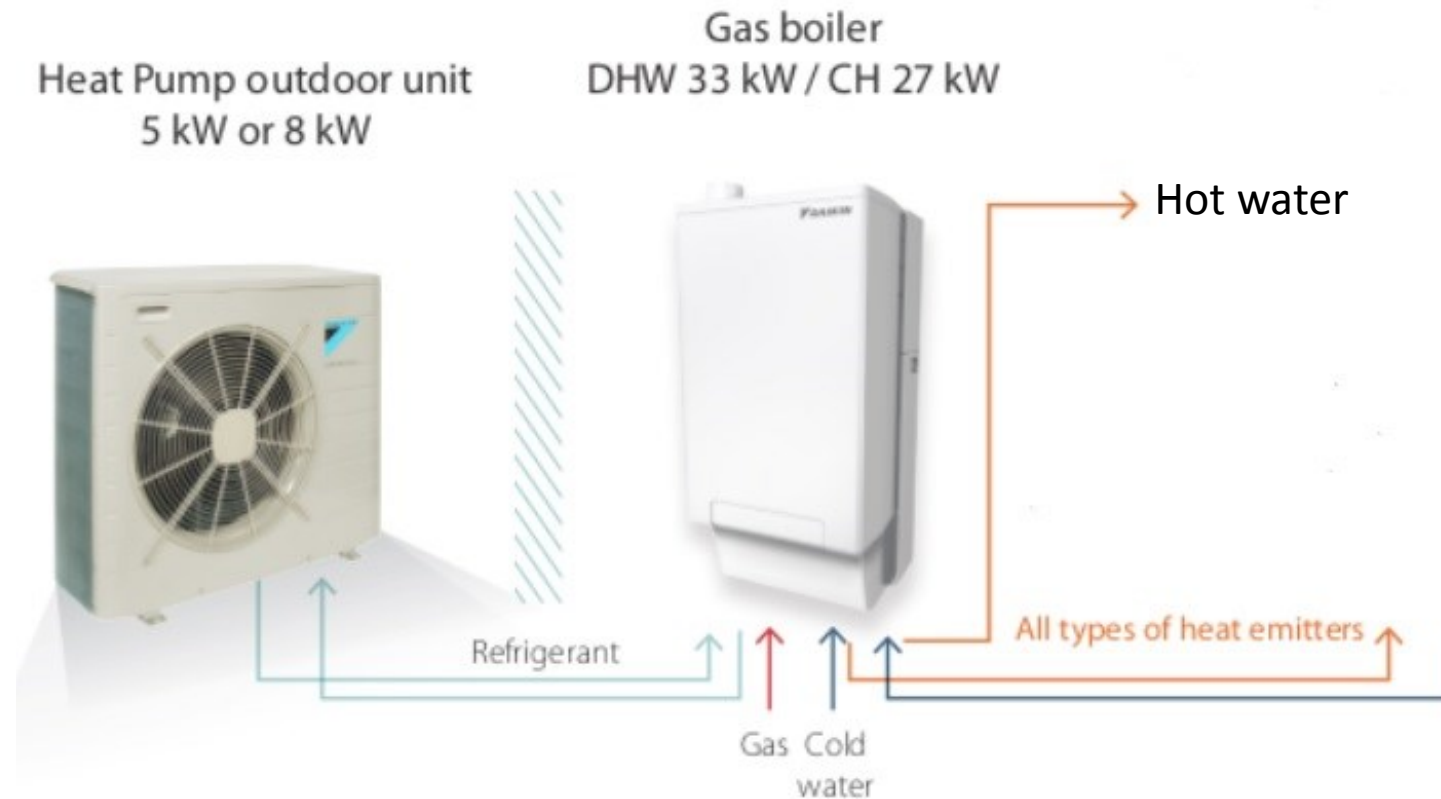


# Smart thermal storage to alleviate grid stress



Hybridisation of phase change material in a water storage tank

# Hybridisation – an interim way forward?

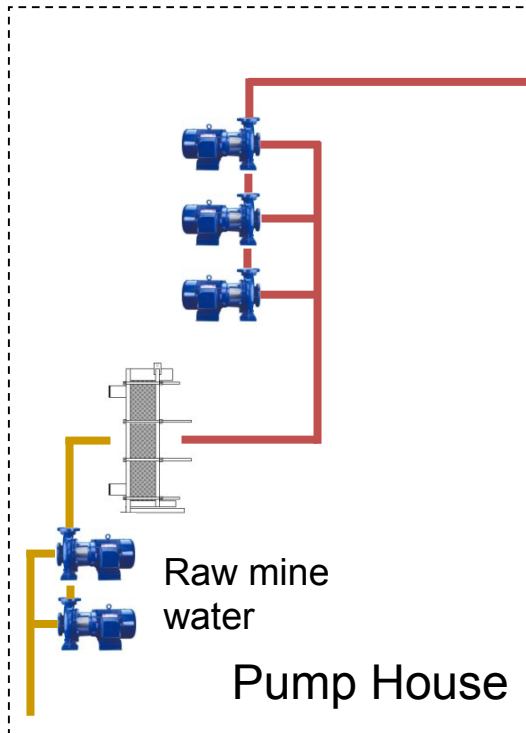
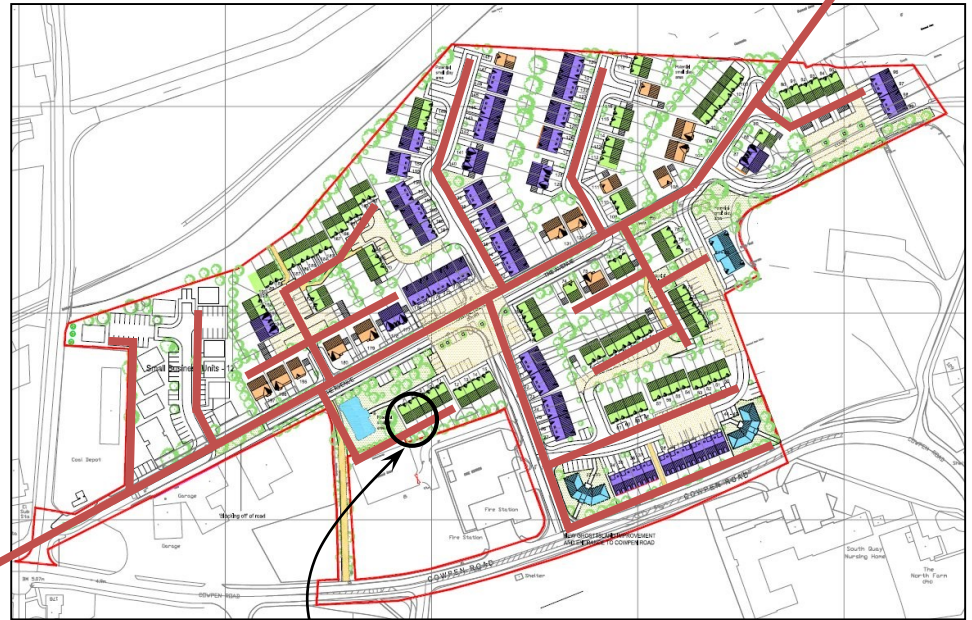


# Large scale applications – district sourcing by mine dewatering

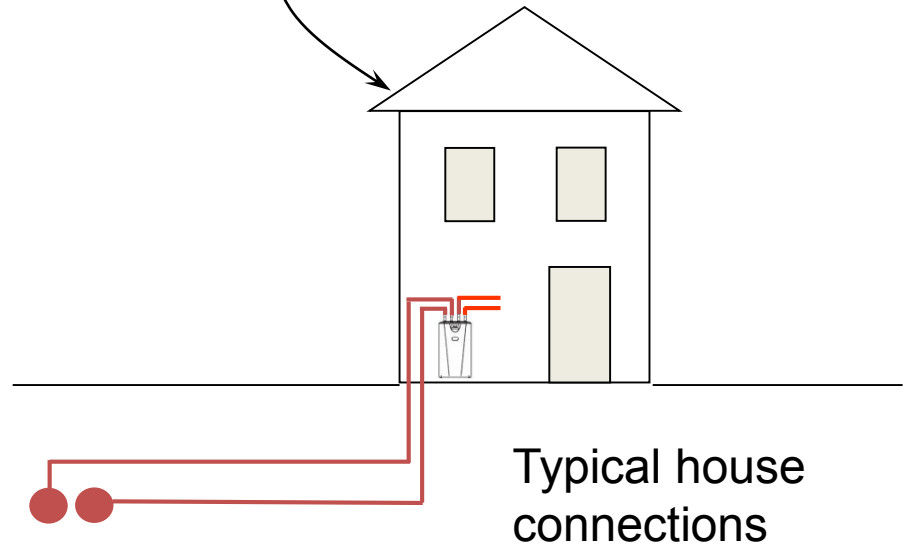


Thoroton and Croft Estate, Blyth

**Option 1: DISTRIBUTED SOURCE**  
**(Independent Heating)**



Source water circuit



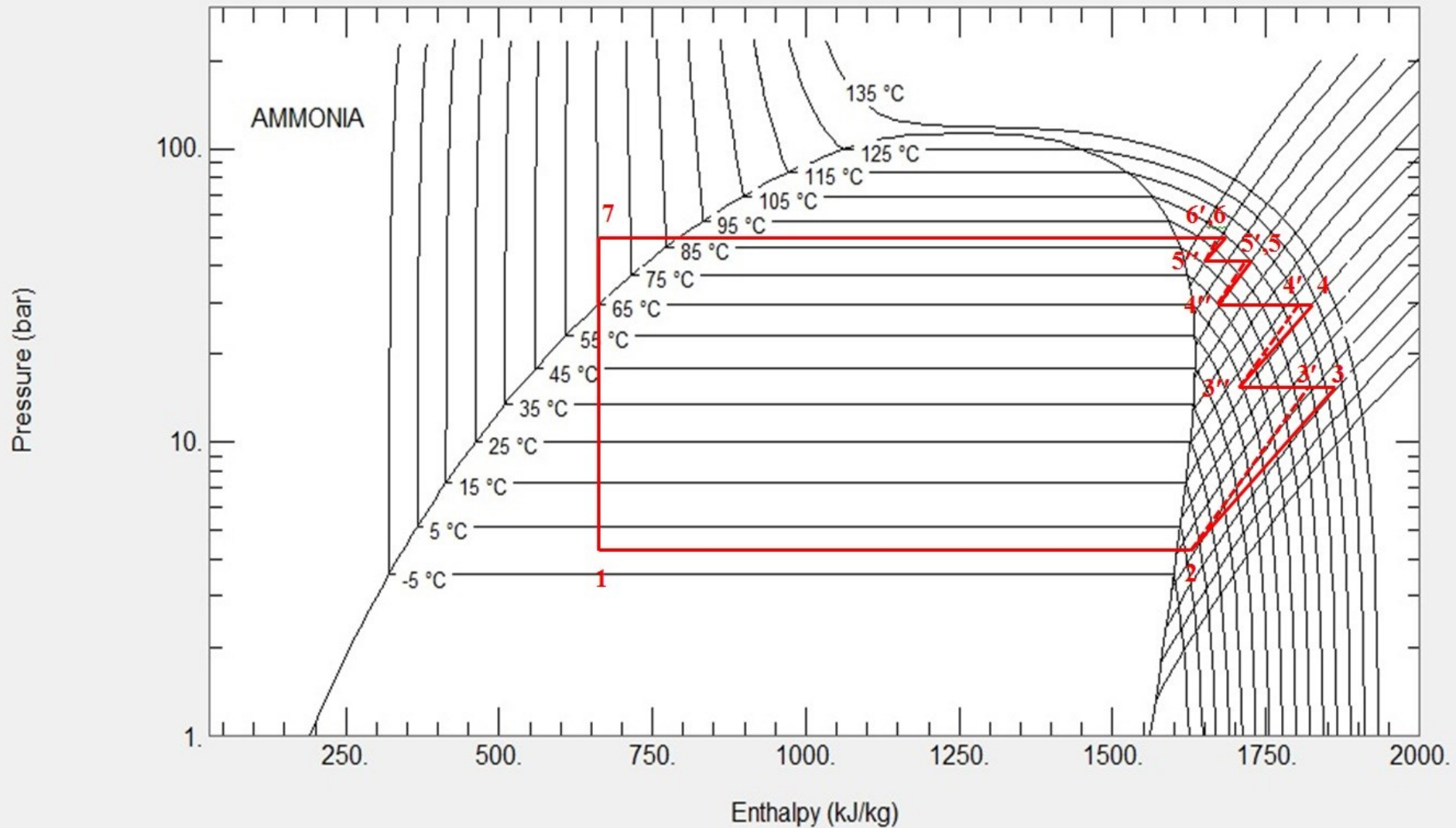
# Heat networks – the Drammen fjernvarme heat pump...

- The Drammen fjernvarme district heating plant in Norway hosts the world's largest seawater source heat pump plant
- Total capacity 14MW based on 3 multistage single-screw compressor ammonia heat pumps generating hot water at 90°C (peak) flow, 60°C return generating 67GWh of heat per year
- Single-screw compressors used with a maximum discharge temperature of 135°C; the cycle for this high lift application is managed through a series of compression stages each followed by a desuperheat (and oil cooling) process
- Single screw compressors used because they are expected to enjoy longer bearing life than their more efficient twin-screw counterparts
- Source: north sea water from the Oslo fjord, drawn 18m below the seawater surface at constant year-round temperatures of 8-9°C (4°C evaporator outlet temperature)
- Operating pressures 4.4bar (evaporating – superheated to 6°C); 26bar (intermediate) and 50bar (condensing – sub-cooled to 65°C) – the three heat pumps are connected in series hence these conditions are nominal

Further reading...

<http://www.ammonia21.com/web/assets/link/Hoffman7thApril2011London%20colour.pdf> (accessed November 2015)

# 'High lift' heat pump cycle for use with heat networks



## And, finally, economics: The UK's Renewable Heat Incentive – a financial 'leg up' for heat pumps and other thermal technologies...

- Launched in 2011 (non-domestic) and 2014 (domestic)
- Tariff support for a range of renewable heat emitter systems to incentivise take-up of these new technologies
- From 1<sup>st</sup> July 2017 in the non-domestic RHI, ground- and water-source heat pumps receive a tariff payment of 9.09p/kWh (for the first 15% of full load equivalent hours 'FLEH') and 2.71p/kWh (for the remainder) applicable to the renewable (source) heat only and payable for 20 years
- The tariff for air-to-water heat pumps is 2.71p/kWh and strictly for heat pumps (i.e. reverse cycle heat pumps with summer cooling are ineligible)
- The tariff payments in the domestic RHI are 7.63p/kWh (air-source) and 19.64p/kWh (ground-source) but are payable for just 7 years
- To be eligible, the heat pump must have a minimum *seasonal performance factor (SPF)* of 2.5 (the *SPF* is defined in the same way as the *CoP* but represents a value averaged over the entire heating season)
- Note that the above is subject to change

Further details:

<http://www.ofgem.gov.uk/environmental-programmes>